

EFFECTS OF AN AXISYMMETRIC RIGID PUNCH ON A NONHOMOGENEOUS TRANSVERSELY ISOTROPIC HALF-SPACE

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Abstract

Elastic behaviour of a nonhomogeneous transversely isotropic half-space is studied under the action of a smooth rigid axisymmetric indenter. Hankel transforms of different orders have been used. It is observed that in contrast to a homogeneous medium, the pressure distribution in the contact region in a nonhomogeneous medium is not directly available, rather it is obtainable from the solution of a Fredholm integral equation. The integral equation is solved for a flat-ended punch and paraboloidal indentations for various values of the nonhomogeneity parameter, and the effects of nonhomogeneity in elastic behaviour on stresses have been shown graphically. The results of the associated homogeneous case are readily available from the results of the present study.

1. Introduction

The determination of the elastic displacement field in the half-space under the action of a rigid indenter has been the subject of much interest and various methods have been employed for the solution of such problems: for example, Spence [10, 11] applied the Wiener-Hopf method, and Sneddon [9] obtained a relation between load and penetration for a punch of arbitrary profile using the integral transform method. A systematic description of such works has been given by Gladwell [3]. A solution of the axisymmetric Boussinesq problem for an initially stressed Neo-Hookean half-space has been reported by Dhaliwal and Singh [2]. Ting [12] considered contact stresses between a rigid indenter and a viscoelastic half-space. Most of the works in this field have been limited to isotropic elastic media. But increased use of anisotropic materials in engineering applications has resulted in considerable attention being focused on media of anisotropic character. Some works in this field are available in Gladwell's book [3]. One basic problem that arises in considering an anisotropic

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medium is that, except for some particular types of anisotropy it is not possible to write displacement components in terms of potential functions in a general anisotropic medium (Lekhnitskii [6]). Stress distribution in an anisotropic elastic half-space under axially symmetric normal load has been discussed by Lekhnitskii [6]. More recently, the strain fields in a transversely isotropic half-space have been investigated by Pouyet and Lataillade [8], who used Hankel transforms of different orders to solve the problem.

Positional variation of elastic coefficients leads to a nonhomogeneous elastic medium, which is a very important concept from a practical point of view. But this area has not been studied rigorously possibly due to the severe difficulty in handling the governing differential equations for such a medium. Sometimes it is observed that even for a comparatively straightforward case of power law variations, the governing equations appear too difficult. It is possible that this is why investigations in this area have thus far been limited to special types of variations in elastic coefficients (see, for example, [1, 5, 7]), rather than consideration of general variations.

The present study focuses on the determination of elastic strains, penetration depth and pressure distribution *etc.* in a nonhomogeneous transversely isotropic half-space caused by a rigid punch. Nonhomogeneity in elastic coefficients c_{ij} has been assumed in the form $c_{ij} = c_{ij}^0 e^{\alpha z}$, α being a real constant. As in [8], Hankel transforms of different orders have been applied to find the solution. In contrast to the homogeneous case, the equation for pressure distribution is a Fredholm integral equation of the second kind. The integral equation has been solved numerically and the stresses have been computed. The effects of nonhomogeneity on stresses have been represented graphically for some special cases of indentation. Finally, all the results for the homogeneous medium may be obtained from the results of the present discussion by putting $\alpha = 0$.

2. The basic equations

We consider an elastic half-space of transversely isotropic material and suppose that the plane of isotropy passing through each point of the body is parallel to the plane boundary of the half-space. Taking the z -axis along the normal to the half-space boundary and pointing inwards and using cylindrical coordinates (r, θ, z) , the stress-strain relations are given by $[\sigma_r, \sigma_\theta, \sigma_z, \sigma_{rz}]^T = [C^*][\varepsilon_r, \varepsilon_\theta, \varepsilon_z, \varepsilon_{rz}]^T$, where $[C^*]$ is the elastic coefficient matrix such that

$$[C^*] = \begin{pmatrix} c_{11} & c_{12} & c_{13} & 0 \\ c_{12} & c_{11} & c_{13} & 0 \\ c_{13} & c_{13} & c_{33} & 0 \\ 0 & 0 & 0 & c_{44} \end{pmatrix}.$$

Because of elastic symmetry and the symmetry of the force distribution the displacement components are independent of θ and we may take

$$u_r = u(r, z), \quad u_\theta = 0, \quad u_z = w(r, z) \quad (2.1)$$

and the strain components related to the displacement components given by (2.1) are

$$\varepsilon_r = \frac{\partial u}{\partial r}, \quad \varepsilon_\theta = \frac{u}{r}, \quad \varepsilon_z = \frac{\partial w}{\partial z}, \quad \varepsilon_{rz} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial r}, \quad \varepsilon_{r\theta} = \varepsilon_{\theta z} = 0. \quad (2.2)$$

The equations of equilibrium are

$$\frac{\partial \sigma_r}{\partial r} + \frac{1}{r}(\sigma_r - \sigma_\theta) + \frac{\partial \sigma_{rz}}{\partial z} = 0, \quad \frac{\partial \sigma_{rz}}{\partial r} + \frac{\sigma_{rz}}{r} + \frac{\partial \sigma_z}{\partial z} = 0. \quad (2.3)$$

We assume that the nonhomogeneity of the elastic medium is due to the dependence of the c_{ij} 's on depth, in the form $c_{ij} = c_{ij}^0 e^{\alpha z}$, where c_{ij}^0 and α are constants.

3. Boundary conditions

Let the tip of the axisymmetric as well as smooth punch penetrate through a depth D (at present unknown) into the half-space. Taking the tip of the punch as the origin, let $z = f(r)$ be the equation of the punch, with the condition that $f(0) = 0$. The function $f(r)$ together with its first derivative is assumed to be continuous, except possibly on the axis.

The boundary conditions for the problem are as follows:

$$\begin{aligned} \sigma_z(r, 0) &= 0, & r > a, \\ \sigma_{rz}(r, 0) &= 0, & \forall r \end{aligned} \quad (3.1)$$

and

$$D - f(r) = w(r, 0). \quad (3.2)$$

Here we assume that a is the radius of the circle of contact.

In addition to the above boundary conditions we must have the obvious regularity conditions that the stresses and displacements should tend to zero as $\sqrt{r^2 + z^2} \rightarrow \infty$.

4. Use of Hankel transforms

Following [8], we use Hankel transforms of different orders with respect to the variable r to express the basic equations and boundary conditions in terms of the single variable z . We shall denote the Hankel transform of order ν of a function $f(r)$ by $\bar{f}(q)$ such that $\bar{f}(q) = \int_0^\infty r f(r) J_\nu(qr) dr$.

In our subsequent analysis we shall apply a Hankel transform of

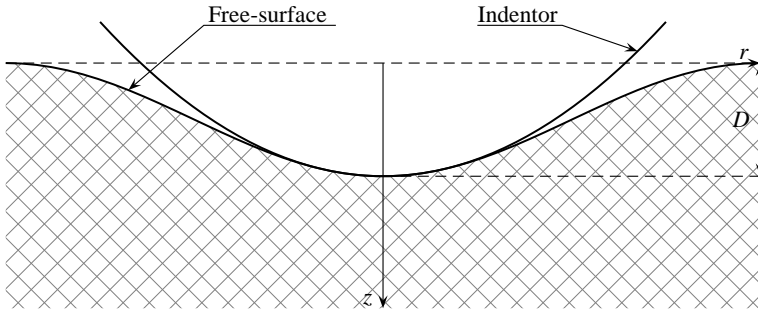


FIGURE 1. Rigid indenter on a half-space.

- (i) zero order to $\sigma_r + \sigma_\theta, \sigma_z, \varepsilon_r + \varepsilon_\theta, \varepsilon_z$ and w ;
- (ii) order one to $\sigma_{rz}, \varepsilon_{rz}$ and u ;
- (iii) order two to $\sigma_r - \sigma_\theta, \varepsilon_r - \varepsilon_\theta$.

Then in terms of the transformed functions the equations of equilibrium (2.3) become

$$q (\overline{\sigma_r - \sigma_\theta}) - q (\overline{\sigma_r + \sigma_\theta}) + 2 \frac{d\bar{\sigma}_{rz}}{dz} = 0, \quad q \bar{\sigma}_{rz} + \frac{d\bar{\sigma}_z}{dz} = 0. \tag{4.1}$$

The stress-strain relations become

$$\begin{aligned} \overline{\sigma_r + \sigma_\theta} &= c_{44} \left[q(a_3 + a_4)\bar{u} + 2a_1 \frac{d\bar{w}}{dz} \right], & \bar{\sigma}_z &= c_{44} \left[qa_1\bar{u} + a_2 \frac{d\bar{w}}{dz} \right], \\ \overline{\sigma_r - \sigma_\theta} &= c_{44}q(a_4 - a_3)\bar{u}, & \bar{\sigma}_{rz} &= c_{44} \left[\frac{d\bar{u}}{dz} - q\bar{w} \right], \end{aligned} \tag{4.2}$$

where

$$\begin{aligned} a_1 &= c_{13}^0/c_{44}^0, & a_2 &= c_{33}^0/c_{44}^0, & a_3 &= c_{11}^0/c_{44}^0, & a_4 &= c_{12}^0/c_{44}^0. \\ \overline{\varepsilon_r + \varepsilon_\theta} &= q\bar{u}, & \overline{\varepsilon_r - \varepsilon_\theta} &= -q\bar{u}, & \bar{\varepsilon}_z &= \frac{d\bar{w}}{dz}, & \bar{\varepsilon}_{rz} &= \frac{d\bar{u}}{dz} - q\bar{w}. \end{aligned} \tag{4.3}$$

If $p(r)$ is the pressure of the punch on $z = 0$, then

$$\sigma_z(r, 0) = -p(r), \quad r \leq a. \tag{4.4}$$

Hankel transforms of boundary condition (3.1) and Equation (4.4) yield

$$\bar{\sigma}_{rz}(q, 0) = 0 \quad \text{and} \quad \bar{\sigma}_z(q, 0) = -\bar{p}(q), \tag{4.5}$$

where

$$\bar{p}(q) = \int_0^a rp(r)J_0(qr) dr. \tag{4.6}$$

5. Method of solution

It can easily be shown by substitution of (4.2) into (4.1) that \bar{u} and \bar{w} satisfy the following linear differential equation in z :

$$\left(\frac{d^2}{dz^2} + \alpha \frac{d}{dz} - q^2 \delta_1^2\right) \left(\frac{d^2}{dz^2} + \alpha \frac{d}{dz} - q^2 \delta_2^2\right) [\bar{u}, \bar{w}] = 0, \tag{5.1}$$

where δ_1 and δ_2 are calculated from

$$\begin{cases} a_2(\delta_1^2 + \delta_2^2) = a_2 a_3 - a_1(2 + a_1), \\ q^2 a_2 \delta_1^2 \delta_2^2 = a_1 \alpha^2 + q^2 a_3. \end{cases} \tag{5.2}$$

In contrast, to the nature of the solution in the homogeneous case ($\alpha = 0$), the solutions of (5.1) are not easily available due to the presence of the nonhomogeneity parameter $\alpha (\neq 0)$.

It is clear from (5.2) that the values of δ_1^2 and δ_2^2 will depend on the transform parameter q and the nonhomogeneous parameter α . It may be easily checked that δ_1^2, δ_2^2 will be real or complex according as

$$\alpha^2 \leq \text{ or } > \frac{q^2 [a_2 a_3 - a_1(2 + a_1)]^2}{4 a_1 a_2} - q^2 \frac{a_3}{a_1}.$$

Hence for a sufficiently large value of α , δ_1^2 and δ_2^2 will assume complex values. Accordingly, separate attention is to be given to solving (5.1).

Since the solution of (5.1) depends on δ_1^2 and δ_2^2 , henceforth we shall represent the solution corresponding to real δ_1^2 and δ_2^2 in part (a) and that corresponding to complex δ_1^2 and δ_2^2 in part (b) of any relevant equation.

Solutions of (5.1) compatible with the regularity condition are

$$\begin{cases} \bar{u} &= A e^{-\lambda_1 z} + B e^{-\lambda_2 z}, \\ \bar{w} &= \frac{q \{ (1 + a_1) \lambda_1 - \alpha a_1 \}}{u_1 - q^2} A e^{-\lambda_1 z} + \frac{q \{ (1 + a_1) \lambda_2 - \alpha a_1 \}}{u_2 - q^2} B e^{-\lambda_2 z} \end{cases} \tag{5.3a}$$

$$\begin{cases} \bar{u} &= e^{-(\alpha/2 + p_1)z} [A' \cos(q_1 z) + B' \sin(q_1 z)], \\ \bar{w} &= e^{-(\alpha/2 + p_1)z} [(m_2 B' - n_2 A') \cos(q_1 z) - (n_2 B' + m_2 A') \sin(q_1 z)], \end{cases} \tag{5.3b}$$

where $\lambda_i = \alpha/2 + \sqrt{\alpha^2/4 + q^2 \delta_i^2}$, $u_i = a_2 \lambda_i (\lambda_i - \alpha)$, $i = 1, 2$; $p_1, q_1 = \sqrt{(\xi_1 \pm \xi_2)/2}$, $\xi_1^2 = (\alpha^2/4 + q^2 \mu_1)^2 + q^4 \mu_2^2$, $\xi_2 = \alpha^2/4 + q^2 \mu_1$, $\mu_1 = (a_2 a_3 - a_1(2 + a_1))/2 a_2$, $\mu_2^2 = (\alpha^2 a_1 + q^2 a_3)/(a_2 q^2) - (a_2 a_3 - a_1(2 + a_1))^2/4 a_2^2$, $m_2 = (t_1 l_1 - k_1 m_1)/(k_1^2 + t_1^2)$, $n_2 = (k_1 l_1 + t_1 m_1)/(k_1^2 + t_1^2)$, $t_1 = \alpha a_2 q_1 - 2 a_2 q_1 (\alpha/2 + p_1)$, $l_1 = \alpha a_1 q - q(1 + a_1)(\alpha/2 + p_1)$, $k_1 = a_2(\alpha/2 + p_1)^2 - a_2 q_1^2 - \alpha a_2(\alpha/2 + p_1) - q^2$, $m_1 = q q_1(1 + a_1)$.

Applying the transformed boundary conditions (4.5) the constants A, B and A', B' are determined as

$$A = A_1 \bar{p}/q, \quad B = -A_2 \bar{p}/q, \tag{5.4a}$$

where

$$A_1 = \frac{(\alpha - \lambda_2)(u_1 - q^2)}{c_{44}^0(\lambda_1 - \lambda_2)(a_2\lambda_1^2 + a_1q^2)}, \quad A_2 = \frac{(\alpha - \lambda_1)(u_2 - q^2)}{c_{44}^0(\lambda_1 - \lambda_2)(a_2\lambda_2^2 + a_1q^2)}$$

and

$$A' = (\bar{p}/q)M_1, \quad B' = -(\bar{p}/q)M_2, \tag{5.4b}$$

where $M_1 = -qs_4/c_{44}^0(s_1s_4 + s_2s_3)$, $M_2 = -qs_3/c_{44}^0(s_1s_4 + s_2s_3)$, $s_1 = qa_1 + a_2n_2(\alpha/2 + p_1) + q_1m_2a_2$, $s_2 = a_2m_2(\alpha/2 + p_1) + a_2q_1n_2$, $s_3 = qn_2 - (\alpha/2 + p_1)$, $s_4 = q_1 - qm_2$.

Hence from (5.3a), (5.3b) and (5.4a), (5.4b) we find that

$$\bar{w}(q, 0) = R^{-1} \bar{p}/q, \tag{5.5}$$

where

$$R = c_{44}^0(a_2\lambda_1^2 + a_1q^2)(a_2\lambda_2^2 + a_1q^2)/[\lambda_1\lambda_2(\lambda_1 + \lambda_2)qa_2(1 + a_1) + \alpha a_1q^3 + \alpha^2qa_1a_2(\lambda_1 + \lambda_2) - \alpha qa_2\lambda_1\lambda_2 - \alpha qa_1a_2(\lambda_1 + \lambda_2)^2] \tag{5.6a}$$

and

$$R = \frac{c_{44}^0}{q} \frac{s_1s_4 + s_2s_3}{n_2s_4 + m_2s_3}. \tag{5.6b}$$

Taking the inverse Hankel transform of (5.5) and noting boundary condition (3.2), we can write

$$D - f(r) = \int_0^a mp(m) \left[\int_0^\infty R^{-1} J_0(qr) J_0(qm) dq \right] dm. \tag{5.7}$$

In contrast to the homogeneous case in which R given by (5.6a) is a pure constant, here R is a function of q and so the inversion of the integral in (5.7) for the function $p(r)$ is not easy. However, it is possible to reduce (5.7) to a Fredholm integral equation for the determination of $p(r)$.

Let us write

$$C = \frac{c_{44}^0(a_2\gamma_1^2 + a_1)(a_2\gamma_2^2 + a_1)}{a_2(1 + a_1)(\gamma_1 + \gamma_2)\gamma_1\gamma_2},$$

where $a_2(\gamma_1^2 + \gamma_2^2) = a_2a_3 - a_1(2 + a_1)$, $a_2\gamma_1^2\gamma_2^2 = a_3$.

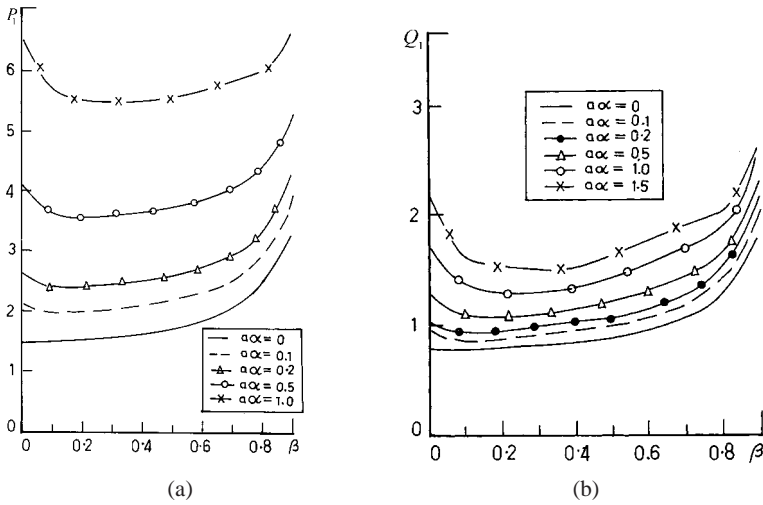


FIGURE 2. Variation of (a) P_1 and (b) Q_1 with β ($\eta = 0$).

Let

$$J(r, m) = \int_0^\infty J_0(qr)J_0(qm) dq = \begin{cases} (2/\pi m)K(r/m), & 0 \leq r \leq m; \\ (2/\pi r)K(m/r), & 0 \leq m \leq r \end{cases}$$

and $T(r, m) = \int_0^\infty (R^{-1} - C^{-1})J_0(qr)J_0(qm) dq$, where K is the complete elliptic integral of the first kind.

Equation (5.7) can be written as

$$D - f(r) = C^{-1} \int_0^a J(r, m)mp(m) dm + \int_0^a T(r, m)mp(m) dm. \tag{5.8}$$

Let us multiply both sides of (5.8) by a factor $\xi/\sqrt{r^2 - \xi^2}$ and integrate as follows:

$$\begin{aligned} \int_0^r \frac{\xi[D - f(\xi)]d\xi}{\sqrt{r^2 - \xi^2}} &= C^{-1} \int_0^r \frac{\xi}{\sqrt{r^2 - \xi^2}} \left[\int_0^a J(\xi, m)mp(m) dm \right] d\xi \\ &+ \int_0^r \frac{\xi}{\sqrt{r^2 - \xi^2}} \left[\int_0^a T(\xi, m)mp(m) dm \right] d\xi. \end{aligned} \tag{5.9}$$

Interchanging the order of integration and using the result [4]

$$\int_0^r \frac{\xi J_0(q\xi) d\xi}{\sqrt{r^2 - \xi^2}} = \frac{\sin(rq)}{q}$$

we get from (5.9) that

$$\int_0^r \frac{\xi[D - f(\xi)]d\xi}{\sqrt{r^2 - \xi^2}} = C^{-1} \int_0^a mp(m) \left[\int_0^\infty \frac{J_0(qm) \sin(rq)}{q} dq \right] dm$$

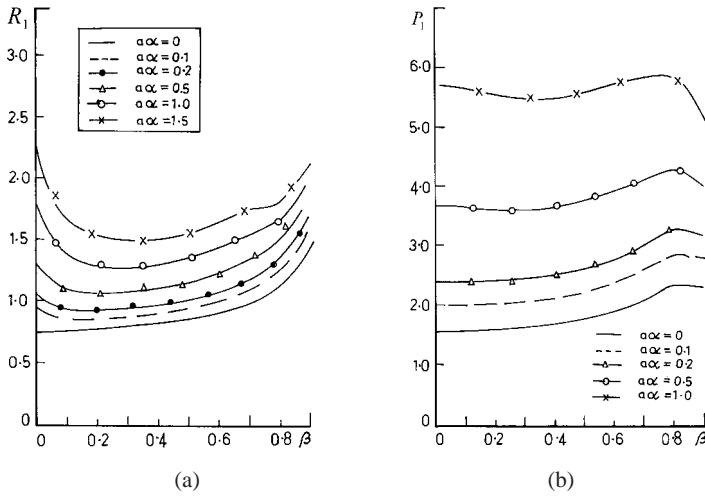


FIGURE 3. Variation of (a) R_1 with β ($\eta = 0$) and (b) P_1 with β ($\eta = 0.2$).

$$+ \int_0^a mp(m) \left[\int_0^\infty \frac{(R^{-1} - C^{-1})J_0(qm) \sin(rq)}{q} dq \right] dm.$$

So we get

$$\begin{aligned} & \frac{\partial}{\partial r} \int_0^r \frac{\xi[D - f(\xi)] d\xi}{\sqrt{r^2 - \xi^2}} \\ &= C^{-1} \int_0^a mp(m) \left[\int_0^\infty J_0(qm) \cos(rq) dq \right] dm \\ &+ \int_0^a mp(m) \left[\int_0^\infty (R^{-1} - C^{-1})J_0(qm) \cos(rq) dq \right] dm. \end{aligned} \tag{5.10}$$

Multiplying (5.10) by a factor as in (5.9) and integrating with respect to r between ζ and a , we get

$$\begin{aligned} & \int_\zeta^a \frac{r}{\sqrt{r^2 - \zeta^2}} \left[\frac{\partial}{\partial r} \int_0^r \frac{\xi[D - f(\xi)] d\xi}{\sqrt{r^2 - \xi^2}} \right] dr \\ &= \int_\zeta^a \frac{r}{\sqrt{r^2 - \zeta^2}} C^{-1} \left[\int_r^a \frac{mp(m) dm}{\sqrt{m^2 - r^2}} \right] dr \\ &+ \int_\zeta^a \frac{r}{\sqrt{r^2 - \zeta^2}} \left[\int_0^a mp(m) \left\{ \int_0^\infty (R^{-1} - C^{-1})J_0(qm) \cos(rq) dq \right\} dm \right] dr. \end{aligned} \tag{5.11}$$

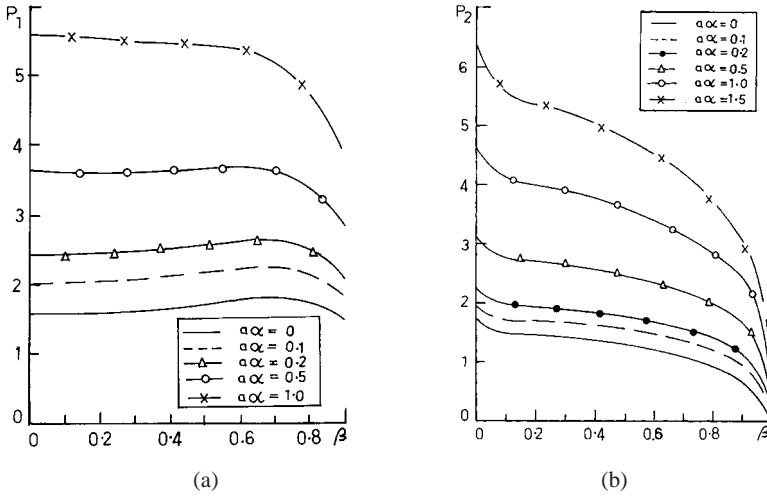


FIGURE 4. Variation of (a) P_1 with β ($\eta = 0.5$) and (b) P_2 with β ($\eta = 0$).

In the derivation of (5.11) we used the following result [4]:

$$\int_0^\infty J_0(qm) \cos(qr) dq = \begin{cases} 1/\sqrt{m^2 - r^2}, & m > r; \\ 0, & m < r. \end{cases}$$

Interchanging the integrals of the first part of the right-hand side and differentiating both sides of (5.11) we get

$$\begin{aligned} & \frac{\partial}{\partial r} \int_r^a \frac{\xi}{\sqrt{\xi^2 - r^2}} \left[\frac{\partial}{\partial \xi} \int_0^\xi \frac{m(D - f(m))}{\sqrt{\xi^2 - m^2}} dm \right] d\xi \\ &= -\frac{\pi}{2C} r p(r) \\ &+ \frac{\partial}{\partial r} \int_r^a \frac{\xi}{\sqrt{\xi^2 - r^2}} \left[\int_0^a t p(t) \int_0^\infty (R^{-1} - C^{-1}) J_0(qt) \cos(q\xi) dq dt \right] d\xi. \end{aligned} \quad (5.12)$$

Let us set $g(r) = D - f(r)$ and

$$G(r) = \frac{\partial}{\partial r} \int_0^r \frac{mg(m) dm}{\sqrt{r^2 - m^2}}, \quad (5.13)$$

then

$$G(r) = g(0) + \int_0^r \frac{rg'(m) dm}{\sqrt{r^2 - m^2}}.$$

Using (5.13), (5.12) may be written as

$$\frac{2C}{\pi} \left[\frac{G(a)}{\sqrt{a^2 - r^2}} - \int_r^a \frac{G'(\xi) d\xi}{\sqrt{\xi^2 - r^2}} \right]$$

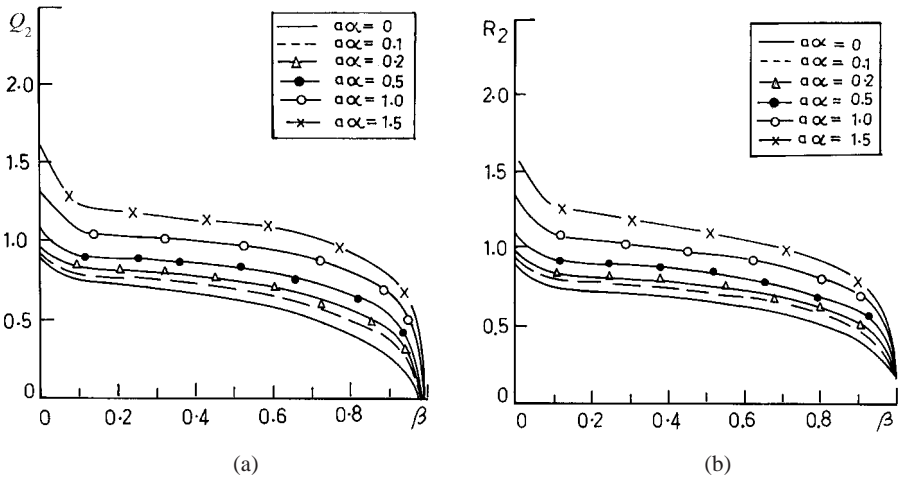


FIGURE 5. Variation of (a) Q_2 and (b) R_2 with β ($\eta = 0$).

$$= p(r) - \frac{2}{\pi r} \frac{\partial}{\partial r} \int_r^a \frac{\xi}{\sqrt{\xi^2 - r^2}} \left[\int_0^a t p(t) f_1(t, \xi) dt \right] d\xi, \tag{5.14}$$

where $f_1(t, \xi) = \int_0^\infty (CR^{-1} - 1) J_0(qt) \cos(q\xi) dq$.

Equation (5.14) can now be put in the form

$$p(r) + \int_0^a L(r, t) p(t) dt = \psi(r), \tag{5.15}$$

where

$$L(r, t) = \frac{2t}{\pi} \left(\frac{f_1(t, a)}{\sqrt{a^2 - r^2}} + \int_r^a \frac{1}{\sqrt{\xi^2 - r^2}} \int_0^\infty (CR^{-1} - 1) q J_0(qt) \sin(q\xi) dq d\xi \right)$$

and

$$\psi(r) = \frac{2C}{\pi} \left[\frac{G(a)}{\sqrt{a^2 - r^2}} - \int_r^a \frac{G'(\xi) d\xi}{\sqrt{\xi^2 - r^2}} \right].$$

The Fredholm integral equation (5.15) will determine $p(r)$ for a known punch profile $f(r)$, consequently the transformed function $\bar{p}(q)$ is known from (4.6). Hence all the transformed functions corresponding to displacements and stresses are known and the problem reduces to that of finding the inverse Hankel transforms of those functions.

We can determine the penetration depth D of the tip of a smooth profile from the condition $p(a) = 0$ as follows. From (5.14), $p(a) = 0$ implies $G(a) = 0$, which gives after some calculations $D = \int_0^a (af'(r)/\sqrt{a^2 - r^2}) dr$, which is the same as in the homogeneous case [8]. We note here that the smoothness condition is not satisfied

in the case of a flat-ended cylindrical punch as pointed out in [9] and so the condition $p(a) = 0$ cannot be used there.

The displacement components are given by

$$u(r, z) = \int_0^\infty \bar{p} [A_1 e^{-\lambda_1 z} - A_2 e^{-\lambda_2 z}] J_1(qr) dq, \quad (a)$$

$$u(r, z) = \int_0^\infty \bar{p} e^{-(\alpha/2+p_1)z} [M_1 \cos(q_1 z) - M_2 \sin(q_1 z)] J_1(qr) dq, \quad (b)$$

$$w(r, z) = \int_0^\infty q \bar{p} \left[\frac{A_1 \{(1+a_1)\lambda_1 - \alpha a_1\}}{u_1 - q^2} e^{-\lambda_1 z} - \frac{A_2 \{(1+a_1)\lambda_2 - \alpha a_1\}}{u_2 - q^2} e^{-\lambda_2 z} \right] J_0(qr) dq, \quad (a)$$

$$w(r, z) = - \int_0^\infty \bar{p} e^{-(\alpha/2+p_1)z} [(m_2 M_2 + n_2 M_1) \cos(q_1 z) + (m_2 M_1 - n_2 M_2) \sin(q_1 z)] J_0(qr) dq. \quad (b)$$

The strain components are

$$\varepsilon_r + \varepsilon_\theta = \int_0^\infty q \bar{p} [A_1 e^{-\lambda_1 z} - A_2 e^{-\lambda_2 z}] J_0(qr) dq, \quad (a)$$

$$\varepsilon_r + \varepsilon_\theta = \int_0^\infty q \bar{p} e^{-(\alpha/2+p_1)z} [M_1 \cos(q_1 z) - M_2 \sin(q_1 z)] J_0(qr) dq, \quad (b)$$

$$\varepsilon_r - \varepsilon_\theta = - \int_0^\infty q \bar{p} [A_1 e^{-\lambda_1 z} - A_2 e^{-\lambda_2 z}] J_2(qr) dq, \quad (a)$$

$$\varepsilon_r - \varepsilon_\theta = - \int_0^\infty q \bar{p} e^{-(\alpha/2+p_1)z} [M_1 \cos(q_1 z) - M_2 \sin(q_1 z)] J_2(qr) dq, \quad (b)$$

$$\varepsilon_z = - \int_0^\infty q \bar{p} \left[\frac{A_1 \lambda_1 \{(1+a_1)\lambda_1 - \alpha a_1\}}{u_1 - q^2} e^{-\lambda_1 z} - \frac{A_2 \lambda_2 \{(1+a_1)\lambda_2 - \alpha a_1\}}{u_2 - q^2} e^{-\lambda_2 z} \right] J_0(qr) dq, \quad (a)$$

$$\varepsilon_z = \int_0^\infty \bar{p} e^{-(\alpha/2+p_1)z} \left[\{(\alpha/2 + p_1)(m_2 M_2 + n_2 M_1) - q_1(m_2 M_1 - n_2 M_2)\} \cos(q_1 z) + \{(\alpha/2 + p_1)(m_2 M_1 - n_2 M_2) + q_1(m_2 M_2 + n_2 M_1)\} \sin(q_1 z) \right] J_0(qr) dq, \quad (b)$$

$$\varepsilon_{rz} = - \int_0^\infty \frac{\bar{p}(\lambda_1 - \alpha)(\lambda_2 - \alpha)}{c_{44}^0(\lambda_2 - \lambda_1)} [e^{-\lambda_1 z} - e^{-\lambda_2 z}] J_1(qr) dq, \quad (a)$$

$$\varepsilon_{rz} = \int_0^\infty \bar{p} e^{-(\alpha/2+p_1)z} \left[\left(q(m_2 M_2 + n_2 M_1) - M_1 \left(\frac{\alpha}{2} + p_1 \right) - M_2 q_1 \right) \cos(q_1 z) + \left(q(m_2 M_1 - n_2 M_2) + M_2 \left(\frac{\alpha}{2} + p_1 \right) - M_1 q_1 \right) \sin(q_1 z) \right] J_1(qr) dq \quad (b)$$

and the stress components are

$$\sigma_r + \sigma_\theta = \int_0^\infty q \bar{p} [B_1 e^{(\alpha-\lambda_1)z} - B_2 e^{(\alpha-\lambda_2)z}] J_0(qr) dq, \tag{a}$$

$$\begin{aligned} \sigma_r + \sigma_\theta = c_{44}^0 \int_0^\infty \bar{p} e^{(\alpha/2-p_1)z} & \left[(q(a_3 + a_4)M_1 + 2a_1(\alpha/2 + p_1)(m_2M_2 + n_2M_1) \right. \\ & - 2a_1q_1(m_2M_1 - n_2M_2)) \cos(q_1z) \\ & - (q(a_3 + a_4)M_2 - 2a_1(\alpha/2 + p_1)(m_2M_1 - n_2M_2) \\ & \left. - 2a_1q_1(m_2M_2 + n_2M_1)) \sin(q_1z) \right] J_0(qr) dq \end{aligned} \tag{b}$$

$$\sigma_r - \sigma_\theta = c_{44}^0(a_4 - a_3) \int_0^\infty q \bar{p} [A_1 e^{(\alpha-\lambda_1)z} - A_2 e^{(\alpha-\lambda_2)z}] J_2(qr) dq, \tag{a}$$

$$\sigma_r - \sigma_\theta = c_{44}^0(a_4 - a_3) \int_0^\infty q \bar{p} e^{(\alpha/2-p_1)z} [M_1 \cos(q_1z) - M_2 \sin(q_1z)] J_2(qr) dq, \tag{b}$$

$$\sigma_z = - \int_0^\infty \frac{q \bar{p}}{\lambda_2 - \lambda_1} [(\lambda_2 - \alpha)e^{(\alpha-\lambda_1)z} - (\lambda_1 - \alpha)e^{(\alpha-\lambda_2)z}] J_0(qr) dq, \tag{a}$$

$$\begin{aligned} \sigma_z = c_{44}^0 \int_0^\infty e^{(\alpha/2-p_1)z} \bar{p} & \left[(qa_1M_1 + a_2(\alpha/2 + p_1)(m_2M_2 + n_2M_1) \right. \\ & - a_2q_1(m_2M_1 - n_2M_2)) \cos(q_1z) - (qa_1M_2 - a_2(\alpha/2 + p_1)(m_2M_1 - n_2M_2) \\ & \left. - a_2q_1(m_2M_2 + n_2M_1)) \sin(q_1z) \right] J_0(qr) dq, \end{aligned} \tag{b}$$

where

$$B_i = c_{44}^0 a_i \left((a_3 + a_4) - 2a_1 \lambda_i \frac{(1 + a_1)\lambda_i - \alpha a_1}{u_i - q^2} \right).$$

6. Special case: flat-ended cylindrical punch

In the special case of a flat-ended cylindrical punch, $f(r) = 0$ and hence we get

$$p(r) + \int_0^a L(r, t) p(t) dt = \frac{2CD}{\pi \sqrt{a^2 - r^2}}.$$

The contact force F is then determined from $F = \int_0^a 2\pi r p(r) dr$.

Finally, it may be checked that the results in the associated homogeneous medium as discussed by Pouyet and Lataillade [8] are easily obtainable by putting $\alpha = 0$ in the corresponding results in our present article.

7. Numerical results

To assess the effects of non-homogeneity on stresses we first specify the nature of indentation $z = f(r)$. In our numerical works we shall consider two types of punches:

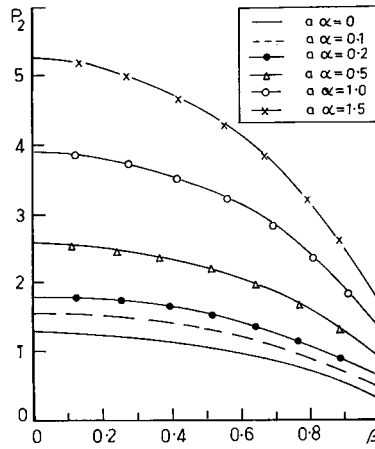


FIGURE 6. Variation of P_2 with β ($\eta = 0.5$).

(a) a flat-ended cylindrical punch for which $f(r) = 0$ and (b) a paraboloidal punch for which $f(r) = r^2/4a$. Numerical computations are done taking various values of the non-homogeneity parameter α as mentioned in the figures. The values of the coefficients a_i in (4.3) are taken for fibreglass epoxy composite material from [8]. The integral equation (5.15) is solved numerically to determine the pressure $p(r)$, which is subsequently used to determine the non-dimensional stress components.

For a flat-ended cylindrical punch we have shown variations of $P_1 = -a\sigma_z/(Dc_{44}^0)$, $Q_1 = -a\sigma_r/(Dc_{44}^0)$, $R_1 = -a\sigma_\theta/(Dc_{44}^0)$ for different values of $\beta = r/a$ and $\eta = z/a$ in Figures 2–4 (a).

For the paraboloidal punch we have represented variations of $P_2 = -\sigma_z/c_{44}^0$, $Q_2 = -\sigma_r/c_{44}^0$, $R_2 = -\sigma_\theta/c_{44}^0$ for different values of β and η in Figures 4 (b)–6. The effects are quite clear from the figures.

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